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Research Article

Performance Analysis of Ammonia Converter in Ammonia Unit Factory

Evaluasi Kinerja Ammonia Converter Pada Pabrik Unit Amonia

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*Corresponding Author. Email:	Abstract				
*Corresponding Author. Email: prahady.susmanto@ft.unsri.ac. id	An ammonia converter is a catalyzed reactor that facilitates the synthesis of NH ₃ (ammonia) from hydrogen (H ₂) and nitrogen (N ₂). Several studies have shown that the performance of this reactor significantly influences the operational efficiency and productivity of ammonia plants. Therefore, this study aims to evaluate the performance of an ammonia converter by assessing the effect of operating conditions on the reactant conversion and reaction products using design and actual data. The operating conditions examined included temperature, pressure, ratio of reactants, and inert mole utilized during the NH ₃ synthesis process. The results showed that the highest NH ₃ yield of 20.28% was achieved in actual data with 351.5°C temperature, 154.32 kg/cm ² pressure, 3.58 raw material ratio, and 3.57% inert mole (sixth dataset). The performance efficiency of an ammonia converter can be assessed using temperature, reactant ratio, and inert moles, while the pressure factor was insignificant due to dataset fluctuations. Based on the evaluation results, the converter experienced a decrease in performance due to a discrepancy in the existing operating conditions between the design and actual data.				

Keywords: Ammonia converter; operating conditions; reactor; yield

Abstrak

Ammonia Converter adalah reaktor berkatalis yang berfungsi sebagai tempat proses pembentukan NH_3 (amonia) dari hidrogen (H_2) dan nitrogen (N_2). Reaktor ammonia converter sangat berpengaruh terhadap produktivitas dan efisiensi di pabrik amonia sehingga diperlukan analisis kinerja reaktor. Tujuan penelitian ini untuk mengevaluasi kinerja ammonia converter berdasarkan kondisi operasi terhadap hasil konversi reaktan dan produk reaksi yang dihasilkan dengan ditinjau dari data desain dan data aktualnya. Penelitian ini menganalisis kondisi operasi suhu, tekanan dan rasio reaktan serta inert yang dihasilkan dari proses sintesis NH_3 dengan membandingkan data aktual yang didapatkan dengan data desainnya. Hasil evaluasi menunjukkan kondisi operasi optimal yang dicapai oleh NH_3 converter dengan suhu 154,32°C, tekanan 154,32 kg/cm², rasio reaktan 3,58 dan mol inert 3,57% dengan konversi H_2 32,82%, konversi N_2 35,11% dan yield NH_3 20,28%. Hasil evaluasi menujukkan efisiensi kinerja reaktor ammonia converter dapat ditinjau oleh suhu, rasio reaktan dan mol inert sedangkan faktor tekanan tidak dapat digunakan karena data aktualnya yang fluktuatif. **Kata kunci** : Ammonia converter; kondisi operasi; reaktor; yield

1. Introduction

Ammonia synthesis is a process that is often carried out in an ammonia converter unit. Within this unit, synthesis gases $(N_2 \text{ and } H_2)$ obtained from the purification unit are reacted to obtain ammonia based products [1]. Furthermore, it is indigenously structured with three horizontal bed converters, which are designed using pressure wall materials at a cold temperature. The cold feed gas is passed through the annulus between the catalyst basket and the converter wall to maintain a low wall vessel temperature [2,3]. The converter unit also consists of a removable basket containing 4 fixed beds and 2 interchangers, with approximately 77.1 m^3 of promoted iron catalyst [3]. The volume of the catalyst within the beds varies, and it increases from the first to the third bed. This strategic volume augmentation helps curtail to the temperature elevation caused by the exothermic reaction occurring within the first bed (where the fastest reaction occurs). Consequently, the design preserves the converter's temperature within the desired range [3,4]. The ammonia formation is an exothermic equilibrium reaction using the Haber-Bosch process method, which is illustrated below [1]:

 $N_{2(g)} + 3H_{2(g)} \implies 2NH_{3(g)}$ (1)

The performance of an ammonia converter is significantly influenced by several factors, including temperature, pressure, H_2/N_2 ratio, and inert mole. Several studies have shown that temperature plays a dual role, impacting both the synthesis reaction rate and ammonia equilibrium. NH₃ synthesis occurs through an exothermic reaction, leading to the limitation of the operating temperature by chemical equilibrium. However, higher levels concurrently enhance kinetic energy, leading to faster molecular collisions [5].

Pressure is a crucial factor that influences both the equilibrium of NH_3 and reaction rate, where higher levels often lead to increased yield. Changing the H_2/N_2 ratio can lead to an increase or decrease in yield in an ammonia converter. Based on the plant design, an optimal H_2/N_2 ratio typically ranges from 2.8-3.2 [2–4]. The primary operational variable used to control the hydrogen and nitrogen ratio is the composition of the introduced make-up or fresh feed gas.

Methane and argon are inert components commonly found within the syngas stream. These components are not harmful to the catalyst and do not undergo synthesis reactions. However, they have been reported to have a negative impact on reaction rates and equilibrium. A feasible approach that is often used to minimize inert concentration involves purging syngas in the loop [1,3,4]. Therefore, this study aims to analyze the performance of an ammonia converter in an NH₃ plant by comparing the yield obtained under actual and standard operating conditions. The parameters observed included temperature, pressure, reactant ratio, and the inert mole produced by the reactor.

2. Research Methods

The methodology used in this study included a literature review, observation, as well as data collection and processing. The dataset used for the ammonia converter analysis consisted of both design and actual data. The design dataset included the predetermined parameters established during the development of the unit [2,4]. Furthermore, these parameters consisted of inlet temperature, pressure, inert mole, and H_2/N_2 reactant ratio.

3. Results and Discussion

The actual data used for evaluating the performance of an ammonia converter from were obtained the operation conditions at the control room and laboratory of the PT PUSRI IIB unit in the form of log sheets. The conditions examined included the flow rate, %mol composition data for inlet and outlet, feed temperature, pressure, inter-bed temperature, inert mole, and H₂/N₂ reactant ratio. Furthermore, the analysis was performed with mass balance calculations using Microsoft Excel to determine the conversion of N₂ and H₂. It was also used to determine the yield of NH₃ products produced by comparing the design and actual data. The actual data from 6th December 2021 to 31th January 2022, were used, totaling 9 dataset points.

Table 1 shows the results of H_2 and N_2 reactant conversion as well as NH_3 yield based on the operating conditions of temperature, pressure, reactant ratio, and inert mole. The data were then plotted as a graph in Figure 1 to observe the midpoint of the dataset points based on the conditions

influencing the reactant conversion and product yield. Polynomial regression was performed on the data in Table 1 to determine the optimal relationship between temperature, pressure, reactant ratio, and an inert mole in the conversion of H_2 and N_2 into NH₃.

In Figure 1, there was a convergence point of the four sets of operating conditions, which was indicated by the 6th dataset. This suggested that the optimal operating conditions affecting the NH₃ production process were achieved with the 6th data, namely 351.25 °C temperature, 154.32 kg/cm² pressure, 3.58 reactant ratio, and 3.57% inert mole.

Based on polynomial regression Figure 2 showed results. а similar intersection point to Figure 1, which was achieved at the 6th operating data point. This indicated the occurrence of synchronization between the factors affecting the NH_3 process, namely temperature, pressure, reactant ratio, and inert mole. The conversion results obtained were 32.82% conversion of H₂, 35.11% conversion of N₂, and 20.28% yield of NH₃.

Data	Inlet Temp. (°C)	Inlet Press.	H2/N2 Ratio	Inert (%mol)	Energy Gibbs	H ₂ Conversion	N ₂ Conversion	NH3 Yield
	. ,	(kg/cm²)			(KJ/KMOI)	(%mol)	(%mol)	(%mol)
1	349,50	151,84	3,20	3,78	-165,9	30,00	33,11	19,56
2	349,31	152,57	3,31	3,68	-165,9	30,85	34,30	19,92
3	349,34	153,40	3,37	3,63	-165,9	28,41	36,66	20,10
4	347,73	153,61	3,57	3,61	-165,6	32,91	34,15	19,89
5	347,56	155,02	3,34	3,78	-165,6	29,04	36,11	20,11
6	351,25	154,32	3,58	3,57	-166,3	32,82	35,11	20,28
7	348,42	154,45	3,55	3,68	-165,7	30,57	35,71	20,05
8	347,75	154,80	3,43	3,57	-165,6	25,00	38,66	19,78
9	349,25	154,40	3,26	3,80	-165,9	31,13	33,61	20,03
Design	380,00	157,90	3,00	3,50	-171,8	32,55	32,44	20,31

Table 1. Ammonia Converter Operating Conditions: Design and Actual Data

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Figure 1. Comparison of temperature, pressure, reactant ratio, and inert mol toward operating data 1-9



Figure 2. Comparison of H₂ conversion, N₂ conversion, and NH₃ yield toward operating data 1-9

The optimal temperature in this study was 351.25° C, leading to an NH₃ yield of 20.28% and an H₂ reactant conversion of 32.82%, which were the highest actual data. This study showed that the actual dataset results were similar to the design results, as shown in Table 1. Furthermore, high reaction temperatures could yield high reactant conversion and product yield [6]. Operations at high levels often accelerated the reaction process and increase the conversion of H₂, N₂, and mole NH₃ [7]. However, processes at high temperatures could shorten the catalyst lifespan by causing faster saturation and decreasing the NH₃ equilibrium degree in the reaction [8].

Inlet temperature affected the NH₃ yield through two factors, including chemical equilibrium and chemical kinetics. Based on chemical equilibrium, the effect of these factors was governed by Le Chatelier's principle. The principle stated that a system in equilibrium, when affected shifted externally, to form а new equilibrium to minimize the external effect This indicated that the operating [9].

temperature in exothermic reactions was limited by chemical equilibrium. When the levels exceeded the threshold, productivity decreased, and product decomposition into reactants occurred to reach a balance [10]. Therefore, the operating temperature in the NH₃ reaction must be maintained within the desired range.

The decrease and increase in NH₃ yield with temperature could be attributed to the energy involved in the reaction process, specifically Gibbs energy [11]. Gibbs energy is a measure of the potential work of a reversible reaction or the maximum work possible for a system at a constant temperature or pressure [11, 12]. Furthermore, it was often used to assess the spontaneity of a reaction. Equilibrium occurred when its value was zero, and there was no reaction if the value was greater than zero. This indicated that the smaller the generated Gibbs energy, the higher the negativity, leading to increased spontaneity [13].

Factors in chemical reaction kinetics were related to the rate of reaction. Higher temperatures often led to faster reactions, leading to an increase in product formation [14]. This was because higher temperatures led to more frequent particle movement, thereby increasing collision frequency and rate [15]. Therefore, increasing the levels within the equilibrium limit could enhance the NH₃ product yield. For the Haber-Bosch synthesis of NH₃, the chemical equilibrium limit occurred at a temperature of 495°C [13].

Decreases in yield were also affected by catalyst performance in each bed and interchanger performance. A lower inlet temperature for an ammonia converter increased the load on the interchanger to raise the level to the desired range. This was because an ammonia converter reaction was exothermic, indicating that increased the temperature enhanced raw material yield, but decreased the NH3 equilibrium degree in the reaction [16].

Optimal conditions were achieved at the 6th data point with a pressure of 154.32 kg/cm². This actual value was lower compared to the design data of 157.9 kg/cm². The results showed that pressure affected both NH₃ equilibrium and reaction rate [16,17].

The increased pressure was caused by several factors, such as the flow rate of fresh makeup gas, a decrease in converter temperature below the desired range, and changes in the gas composition of the H₂ and N₂ ratios. It could also be caused by an increase in NH₃ content in the recycle gas, an increment in inert content, and catalyst deactivation [18], leading to a reduction in product yield. This aligned with the actual data obtained from the first data point with the lowest pressure of 151.84 kg/cm², which yielded the smallest N₂ conversion at 33.11% and NH₃ mol composition at 19.56%. However, this could not be proven for H₂ conversion data due to its greater fluctuation compared to others.

The optimal reactant ratio of 3.58 was achieved at the 6th data point, which was higher compared to the design dataset of 3. Furthermore, the H_2/N_2 ratio referred to the ratio of H_2 and N_2 inlet for each reactant. In the 6th data point, with a value of 3.58, the H_2 conversion was closest to the design data. This corresponded to the highest NH₃ yield obtained from the actual data at 20.28%.

The relationship between the H_2/N_2 reactant ratio and NH_3 yield was related to concentration. According to Le Chatelier's principle, when the equilibrium system experienced an increase in concentration on one side, the equilibrium shifted to the

opposite side [19]. Therefore, increasing the raw material H_2/N_2 ratio was expected to lead to an increase in NH₃ product yield [20].

During the synthesis process, 3 molecules of H_2 and 1 molecule of N_2 were needed to form 2 molecules of NH_3 . When the H_2/N_2 ratio increased beyond the limit, an imbalance in the reactant ratio occurred [21]. Therefore, control of this parameter was necessary to achieve the desired product yield.

In an ammonia converter, the H_2/N_2 ratio was easier to maintain compared to controlling the temperature and pressure conditions. Furthermore, it could be maintained in the reforming unit, specifically in the secondary reformer, by adjusting the air supply to maintain a closeto-3:1 H_2/N_2 ratio.

 H_2/N_2 ratio greater than 3 could be controlled by increasing the airflow into the secondary reformer to increase N_2 as the feed for an ammonia converter. H_2 and N_2 components were maintained since the reactants flowed into an ammonia converter or as fresh feed gas to be converted into NH₃.

Figures 1 and 2 showed the optimal conditions achieved at the 6th data point, with an actual inert mol of 3.57%, which was the closest to the design value of 3.5%. This inert mole gave the highest NH₃ yield and was closest to the design data at

20.28%. Furthermore, the results showed that an increase in the parameter reduced the total reactant conversion. Although the inert compounds present in an ammonia converter were not catalyst poisons, the percentage of inlet and outlet inert mol increased in actual conditions [21]. The increase in the parameter reduced the amount of raw materials entering an ammonia converter. Changes in the percentage value of inert mol in actual conditions were affected by the performance of the reforming section, which supplied reactants before entering the reactor. Methane carried into the converter was obtained from the reactants in the primary and secondary reformers that were not converted into H₂ raw materials.

4. Conclusion

In conclusion, the evaluation of the NH₃ reactor performance showed optimal operating conditions, namely 351.25° C temperature, 154.32 kg/cm^2 pressure, 3.58 reactant ratio, and 3.7% inert mol. These operating conditions gave the highest NH₃ yield at 20.28%, with 32.82% H₂ conversion and 35.11% N₂ conversion. However, the pressure factor was difficult to evaluate due to the fluctuating and unstable data obtained.

References

- [1] Qian, J., An, Q., Fortunelli, A., Nielsen, R. J., & Goddard, W. A. (2018). Reaction Mechanism and Kinetics for Ammonia Synthesis on the Fe(111) Surface. *Journal of the American Chemical Society*, 140(20), 6288–6297. doi: 10.1021/jacs.7b13409
- [2] Siringo-ringo, N. O., Sari, I., & Selpiana. (2019). Evaluasi kinerja ammonia converter pabrik urea ditinjau dari konversi N2 dan H2 dengan menggunakan hysys. *Jurnal Teknik Kimia*, 25(3), 80–85. doi: 10.36706/jtk.v25i3.133
- [3] Agustria, R. M. Y., Al-Azhar., & Putri, R. W. (2019). Evaluasi efisiensi ammonia converter unit ammonia pada industri pupuk urea. *Jurnal Teknik Kimia*, 25(3), 70–74. doi: 10.36706/jtk.v25i3.130
- [4] Rahmatullah, Caesaranty, P. F., & Sari, P. F. (2019). Evaluasi performance ammonia converter

Pabrik urea ditinjau dari pengaruh temperatur, tekanan, rasio H_2/N_2 , dan mol inert inlet, serta perhitungan neraca massa dan neraca panas dengan simulator. *Jurnal Teknik Kimia*, 25(1), 21–30. doi: 10.36706/jtk.v25i1.17

- [5] Abdurrakhman, S., & Hidayat, M. (2012). Studi Simulasi pada Unit Reformer Primer di PT Pupuk Sriwidjaya Palembang. *Jurnal Rekayasa Proses*, 6(2), 30.
- [6] Akpa, J. G., & Raphael, N. R. (2014). Optimization of an Ammonia Synthesis Converter. *World Journal of Engineering and Technology*, 02(04), 305–313. doi: 10.4236/wjet.2014.24032
- [7] Peng, P., Chen, P., Schiappacasse, C., Zhou, N., Anderson, E., Chen, D., ... Ruan, R. (2018). A review on the non-thermal plasma-assisted ammonia synthesis technologies. *Journal of Cleaner Production*, 177, 597–609. doi: 10.1016/j.jclepro.2017.12.229
- [8] Klaas, L., Guban, D., Roeb, M., & Sattler, C. (2021). Recent progress towards solar energy integration into low-pressure green ammonia production technologies. *International Journal of Hydrogen Energy*, 46(49), 25121–25136. doi: 10.1016/j.ijhydene.2021.05.063
- [9] Uline, M. J., & Corti, D. S. (2006). The ammonia synthesis reaction: An exception to the Le Châtelier principle and effects of nonideality. *Journal of Chemical Education*, 83(1), 138–144. doi: 10.1021/ed083p138
- [10] Demirhan, C. D., Tso, W. W., Powell, J. B., & Pistikopoulos, E. N. (2019). Sustainable ammonia production through process synthesis and global optimization. *AIChE Journal*, 65(7). doi: 10.1002/aic.16498
- [11] Wibowo, B. H., & Abdillah, H. L. (2014). Penentuan Tetapan Kecepatan Dan Suhu Reaksi Untuk Memilih Proses Pembuatan Butadien. *Majalah Sains dan Teknologi Dirgantara*, 9(1), 35–42. Retrieved from

http://jurnal.lapan.go.id/index.php/majalah_sains_tekgan/article/view/2051/1864

- [12] Ozturk, M., & Dincer, I. (2021). An integrated system for ammonia production from renewable hydrogen: A case study. *International Journal of Hydrogen Energy*, 46(8), 5918–5925. doi: 10.1016/j.ijhydene.2019.12.127
- [13] Mao, C., Li, H., Gu, H., Wang, J., Zou, Y., Qi, G., ... Zhang, L. (2019). Beyond the Thermal Equilibrium Limit of Ammonia Synthesis with Dual Temperature Zone Catalyst Powered by Solar Light. *Chem*, 5(10), 2702–2717. doi: 10.1016/j.chempr.2019.07.021
- [14] Aboelkheir, I. M. (2022). An Optimized Chemical and Mechanical Engineering Design of an Ammonia Reactor. *Cognizance Journal of Multidisciplinary Studies*, 2(1), 10–37. doi: 10.47760/cognizance.2022.v02i01.002
- [15] Badescu, V. (2020). Optimal design and operation of ammonia decomposition reactors. *International Journal of Energy Research*, 44(7), 5360–5384. doi: 10.1002/er.5286
- [16] Yancy-Caballero, D., Biegler, L. T., & Guirardello, R. (2015). Optimization of an ammonia synthesis reactor using simultaneous approach. *Chemical Engineering Transactions*, 43, 1297– 1302. doi: 10.3303/CET1543217
- [17] Tripodi, A., Conte, F., & Rossetti, I. (2021). Process Intensification for Ammonia Synthesis in Multibed Reactors with Fe-Wustite and Ru/C Catalysts. *Industrial and Engineering Chemistry Research*, 60(2), 908–915. doi: 10.1021/acs.iecr.0c05350
- [18] Suhan, B. K. M., Hemal, M. N. R, Choudhury, M. A. A. S., & Mazumder, M A. A. (2022). Optimal design of ammonia synthesis reactor for a process industry. *Journal of King Saud University - Engineering Sciences*, 34(1), 23–30. doi: 10.1016/j.jksues.2020.08.004
- [19] Hakiki, M. N., Hidayat, M., & Sutijan, S. (2017). Simulasi Pengaruh Steam-To-Carbon Ratio Dan Tube Outlet Temperature Terhadap Reaksi Steam Reforming Pada Primary Reformer Di Pabrik Amoniak. *Rotor*, 10(2), 58. doi: 10.19184/rotor.v10i2.6393
- [20] Aslan, M. Y., Hargreaves, J. S. J., & Uner, D. (2021). The effect of H2:N2ratio on the NH3synthesis rate and on process economics over the Co3Mo3N catalyst. *Faraday Discussions*, 229, 475–488. doi: 10.1039/c9fd00136k
- [21] Cheema, I. I., & Krewer, U. (2020). Optimisation of the autothermal NH3 production process for power-to-ammonia. *Processes*, 8(1), 1–21. doi: 10.3390/pr8010038